

# Laboratory-based reflectometer using line spectra of an RF-induced gas-discharge lamp in 30- to 200-nm wavelength range

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**Abstract.** A laboratory-based reflectometer designed for characterizing the reflectivity of optical coatings in 30- to 200-nm wavelength range was recently developed at IPOE. An RF-produced gas-discharge light source is applied to generate characteristic lines. The light source is mounted on a grazing incident monochromator with a 146-deg deviation angle between the incident and diffracted arms. By precisely adjusting the toroidal grating inside the monochromator chamber, monochromatic lights are acquired through the exit slit. A collimator mirror and two sets of collimation slits with 2 mm × 2 mm dimension are utilized for reducing the divergence of the beam incident on the sample. A high-precision six-axis translation stage, which allows a heavy sample with a maximum diameter of 100 mm, is used to control positions of the samples and the detector. A chopper disk used both for incident light intensity monitor and signal modulation is placed with an incidence angle of 70 deg relative to the incident light beam. The configuration, adjustment process, and test results of the reflectometer are presented in detail. The experimental reflectivity results for Al/LiF/MgF<sub>2</sub> film obtained from our laboratory and BESSY-II Synchrotron as well as Hefei Synchrotron Light Source are given and compared for demonstrating the reliability of the system. © The Authors. Published by SPIE under a Creative Commons Attribution 4.0 International License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: [10.1117/1.JATIS.8.1.017002](https://doi.org/10.1117/1.JATIS.8.1.017002)]

**Keywords:** laboratory-based reflectometer; gas-discharge lamp; extreme ultraviolet and far ultraviolet; Sc/Si multilayer; Al/LiF/MgF<sub>2</sub> film.

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## 1 Introduction

Optical coatings working in extreme ultraviolet (EUV) and far ultraviolet (FUV) wavelength range are applied widely for applications such as material analysis,<sup>1,2</sup> plasma diagnostics,<sup>3,4</sup> microscopic imaging,<sup>5,6</sup> EUV lithography,<sup>7,8</sup> and astrophysics.<sup>9–11</sup> Among all the applications, astrophysics is of the particular interest of this research. Due to the fact that core optical elements carried on the satellites require reflective films with good performance,<sup>12–14</sup> precision characterization of the dedicatedly designed films becomes extremely crucial to the capability of the optics on the EUV and FUV missions. As one of the fundamental properties, reflectivity of the films has aroused considerable attention and need meticulous measurements by reflectometers.

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Different from x-ray and UV-infrared wavelength ranges for which integrated and standardized commercial reflectometers have already acquired mature technology supports,<sup>15,16</sup> in the EUV and FUV band, most commercial reflectometers cannot satisfactorily meet the specific user requirements, especially in the wavelength range below 105 nm.<sup>17,18</sup>

Reflectometers installed on synchrotron radiation stations provide the most reliable metrology for reflectivity measurements in EUV and FUV band, which are distinguished by their spectral continuity, high-intensity and polarized probe beam as well as excellent angular and spectral resolution.<sup>19–26</sup> However, tests at synchrotron facilities require significant advanced and cumbersome appointment procedures, and the users are allocated only limited beam-time. Such a long turn-around time makes it impossible to test the innovation coatings in-time and is unacceptable for some films having temporal stability issues, such as Al/LiF bilayers. On the other hand, due to the existence of higher diffraction order, reliable approaches are required to suppress higher order effects, such as using absorption filters<sup>25,27</sup> or extra mirrors in the beam path.<sup>20,26,28</sup>

To meet the research needs, laboratory-based reflectometers have been implemented around the world.<sup>29–31</sup> The earliest developments of laboratory EUV reflectometers can be traced back to the 1990s, when Nakayama et al.,<sup>32</sup> Gullikson et al.,<sup>33</sup> and Windt et al.<sup>34</sup> developed reflectometers using laser-produced plasma (LPP) light source. Later on, more and more reflectometers based on LPP light source have been set up in laboratories. However, the usage of LPP light source has some limitations, e.g., the working wavelength range was limited in soft x-ray and EUV bands, and the slight instability from shot to shot would definitely influence the measurement accuracy. Aznárez et al.<sup>35</sup> set up a reflectometer using a gas-discharged light source, which extended the working wavelength range from 50 to 200 nm to test FUV multilayers. But the intensity of the probe beam was relatively weak because of technical limitations.

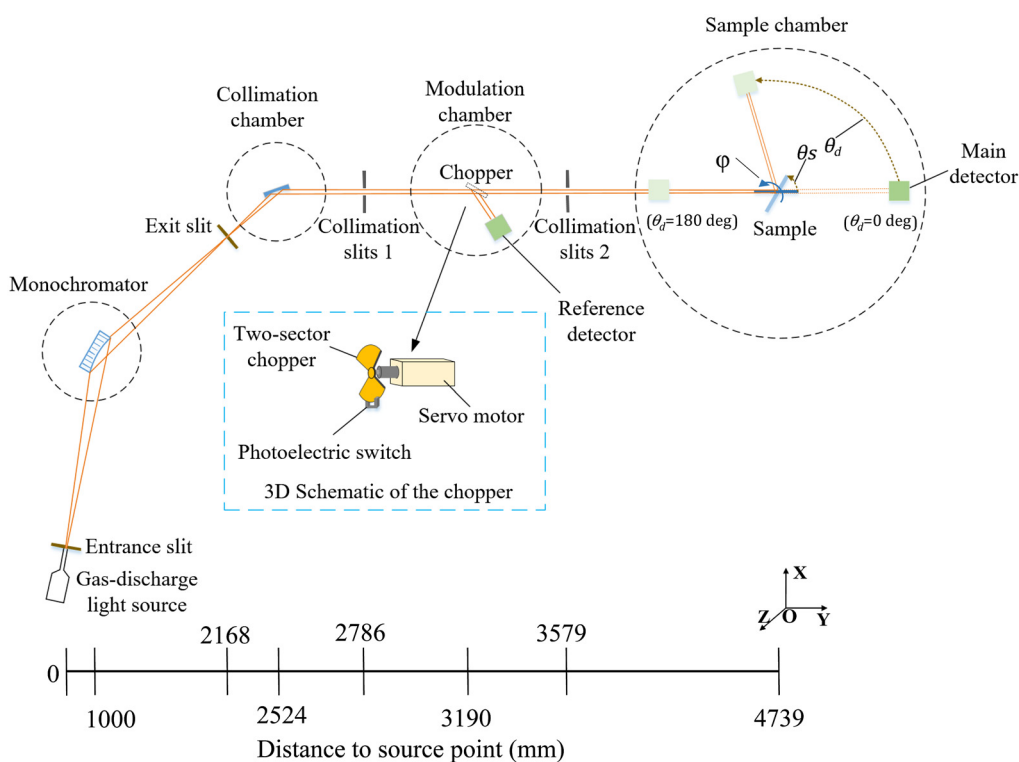
For measuring the reflectivity of films working in EUV and FUV wavelength range, we have implemented a reflectometer utilizing an RF-induced gas-discharge plasma light source, which enjoys the advantages such as high energy coupling efficiency, long working hours, and compatibility with a wide range of experimental conditions, compared with the traditional gas discharge light sources. By changing or mixing the discharging gases, a series of dense characteristic lines covering bands from 30 to 200 nm could be acquired. Presently, only some relative intense characteristic lines of individually discharged gases are applied to perform angular-dependent reflectivity measurements and there are no higher diffraction orders found to overlap with the applied characteristic lines so far. Therefore, the effects of higher orders can be nearly ignored. Thanks to the technique improvement, the light intensity is much stronger and the emitted plasma is limited in a relatively small solid angle. The discharging process generates temporal quasi-continuous light thus the stability of probe beam is much better compared with LPP light source.

In this paper, the reflectometer system is described in detail including the system configuration, the adjusting methods, the measurement procedures as well as the comparison of our measurement results with the data obtained at BESSY-II Synchrotron and Hefei Synchrotron Light Source (HLS) for different samples.

## 2 Description of the Reflectometer

### 2.1 Scheme of the System

The system consists of several basic units as follows: (1) an RF-produced gas-discharge light source, (2) a monochromator with two switchable varied-line-spacing toroidal gratings of 250 and 950 gr/mm, respectively, (3) a collimator chamber, (4) a modulation chamber, and (5) a sample chamber, as showed in Fig. 1. In the following, the structure and the functions of each unit will be explained in detail.

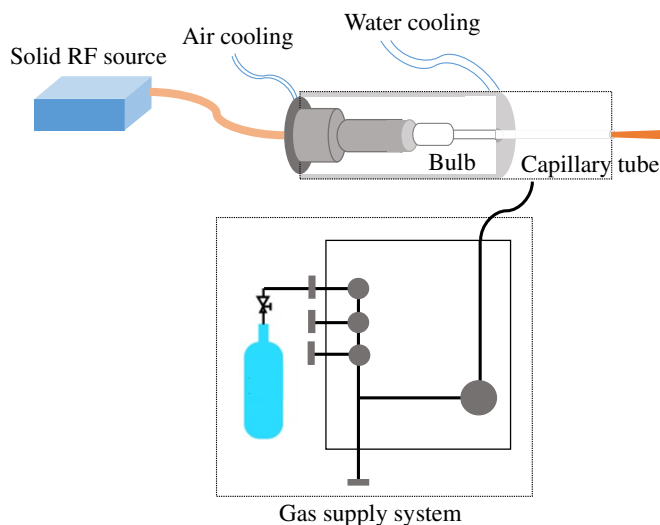


**Fig. 1** Schematic of the reflectometer. The solid orange line represents the optical path. Inside the blue dotted box is a 3D schematic of the chopper disk and the servo motor.

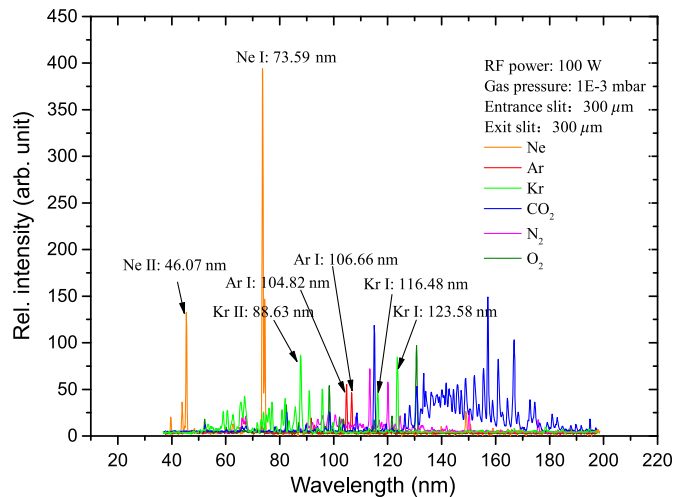
## 2.2 Specific Description of Each Unit

### 2.2.1 Gas-discharge light source

In our system, we adopted an RF-induced gas-discharge lamp (FERMION INSTRUMENTS) based on local field plasma mechanism as the light source, which is electrode-free and ignite-free. A schematic of the lamp, as shown in Fig. 2, shows four parts in general: (1) a solid RF source with the central working frequency of 433 MHz and the maximum power output of 200 W. The optimal working frequency should couple with the position of focused electric field



**Fig. 2** Schematic of the gas-discharge light source.



**Fig. 3** Spectra of several atomic and molecular gases with 300- $\mu\text{m}$  entrance and exit slit of the monochromator.

and should be fine adjusted according to the gas type and working pressure. (2) The capillary design is optimized to the resonant cavity which consists of a bulb and a tube. The bulb is used as the main gas discharge area, and the tube is used as an entrance for the gas inlet and access for the light transmission. (3) Gas supply system which ensures pure gases and controllable gas pressure. (4) Cooling system including water cooling and air cooling.

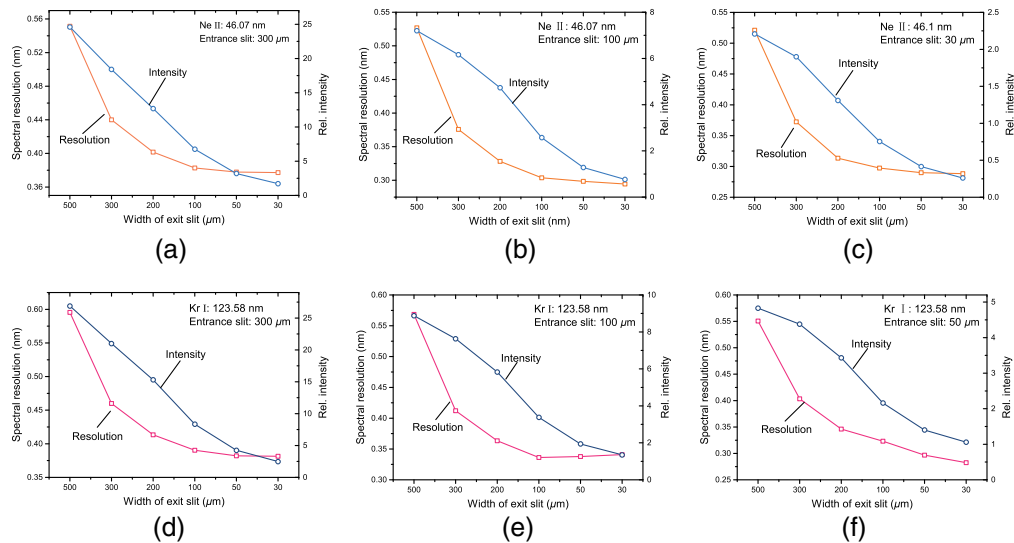
The lamp has a small weight (only 3 kg) and it can accommodate helium, neon, argon, krypton, xenon, nitrogen, oxygen, etc., or a mix of the gases. By measuring the intensity of the exit EUV light beam from the tube, it was estimated that more than  $5\text{E}+12$  photons could be generated per second for Ne II spectral line (46.07 nm and around) when the RF power of 100 W and neon gas pressure of  $2\text{E}-4$  mbar was used. The divergence of the exit light beam is only about 2 deg which is very small and makes it compatible with monochromators. Using the spectral lines or relatively strong continuous spectra of the gases, the reflectometer is able to operate in the wavelength bands from 30 to 200 nm. Such a broad working band is exciting because the probe beam in FUV band is relatively difficult to be acquired in laboratory-based reflectometers.<sup>36</sup> The effect of higher diffraction order can be greatly reduced when only the discrete characteristic lines of the working gases are used for tests.

Figure 3 shows discharging spectra from 30 to 200 nm of several gases including neon, argon, krypton, carbon dioxide, nitrogen, and oxygen. Some strong characteristic lines are marked with the electronic energy level transitions and the corresponding wavelength available in the NIST website. All spectra were measured with the entrance and exit slits of 300  $\mu\text{m}$ .

### 2.2.2 Toroidal grating monochromator

Horiba TGM1200 was adopted as the monochromator with a 1-m focal length and 146 deg deviation angle between the entrance and exit arms. In the chamber, there are two switchable varied-line-spacing gratings working for different wavelength range, one is a 250-gr/mm grating coated with Pt used for 50- to 200-nm wavelength range, while another Au coated grating with line density of 950 gr/mm is of high efficiency in 15- to 50-nm wavelength range.<sup>37</sup> Both gratings are concave toroidal with the slope errors controlled at about 0.2 arc sec both in the directions parallel and perpendicular to the grooves, to ensure excellent performance for correcting aberrations and reducing the quantity of focusing mirrors in the optic path, thus the resolution and throughput of the monochromator can be improved.

In Fig. 4, we studied how the spectral resolution and exit light intensity vary with the slit width of the monochromator. With different configured entrance and exit slit widths, the complete intensity peaks of the characteristic lines are measured by a Si photodiode detector positioned right behind the exit slit. To maintain the spectral scanning with a step of 0.06 nm, the



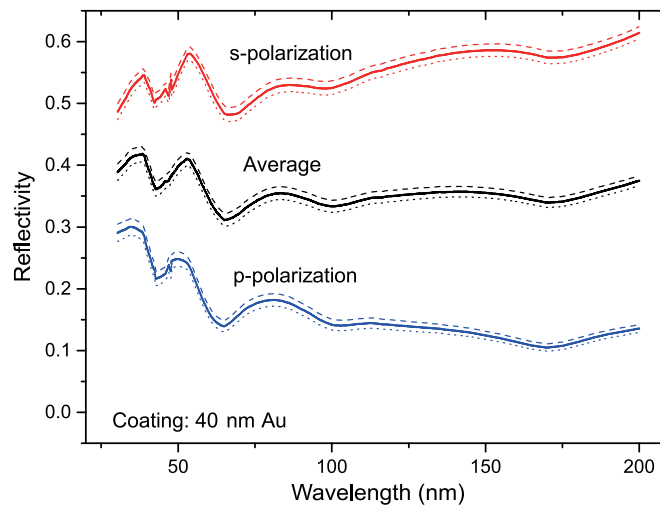
**Fig. 4** Spectral resolution and exit beam intensity variation as a function of exit slit width at 46.07 nm with entrance slit width of (a) 300, (b) 100, (c) 30, and at 123.58 nm with entrance slit width of (d) 300, (e) 100, and (f) 50  $\mu\text{m}$ .

grating rotation and data collection are controlled by a customized LabVIEW program. For each characteristic line, the RF power and gas pressure are required to keep stable during measurement. The spectral resolution as presented by FWHM is deduced by fitting the peaks with a Gauss profile, and the monochromatic light intensities are determined by the peak values. The spectral resolution reaches as high as 0.27 nm at 46.07 nm with 10- $\mu\text{m}$  entrance slit and 30- $\mu\text{m}$  exit slit, and 0.28 nm at 123.58 nm with 50- $\mu\text{m}$  entrance slit and 30- $\mu\text{m}$  exit slit, but the intensity of the exit beam was too weak to be used for reflectivity measurements presently using the photodiode detector. Considering the fact that we used characteristic lines rather than continuous spectra, the width of the slits does not affect the spectral resolution so much. So we adjusted the entrance and exit slit at 300  $\mu\text{m}$  where the spectral resolution moderately decreases to 0.44 nm at 46.07 nm and 0.46 nm at 123.58 nm with the intensity increased by more than 100 times and 20 times, respectively, compared with the situation of the highest resolution. With the entrance and exit slit of 300  $\mu\text{m}$ , the throughput of the monochromator is about  $4.6 \times 10^{10}$  photons per second (PPS) at 46.07 nm and  $8.2 \times 10^9$  PPS at 123.58 nm.

### 2.2.3 Collimation chamber

A collimation chamber is coupled to the monochromator exit flange. Inside this chamber, an Au coated customizing designed toroidal mirror, with 11.3 arc sec slope error in the long side direction and 53.1 arc sec in the short side direction, was mounted on a six-dimensional (6D) adjustment platform. The beam exit from the monochromator is directed onto the mirror with incident angle varied from 69.34 deg to 70.66 deg. Within this incident angle range, the Au film keeps relatively high reflectivity in 30- to 200-nm wavelength region, as shown in Fig. 5. The 6D adjustment platform enables the mirror to be precisely transferred along  $X$  and  $Y$  axis ( $X$  axis is perpendicular to mirror surface and  $Y$  axis is parallel to mirror surface), transferred vertically along  $Z$  axis, rotated with respect to  $Z$  axis, tipped with respect to the  $X$  axis and tilted with respect to the  $Y$  axis. The stability of the platform has been proved by observing the position of the beam using a UV CCD mounted on the sample chamber far away and no obvious shift has been found for several months.

The incident beam is reflected by the collimator mirror with an approximate area of 8 mm  $\times$  8 mm perpendicular to the optical path, which is further collimated by two sets of collimation slits sited at the positions of about 230 and 1260 mm away from the mirror. The collimator mirror and two slits reduced the divergent angle of beam from 1.32 deg to  $-0.01$  deg in meridian direction (in the  $XOY$  plane) and from 1.23 deg to 0.08 deg in sagittal direction (in the  $XOZ$  plane),



**Fig. 5** S-polarized (red lines), p-polarized (blue lines) and average (black lines) reflectivity of Au coating in 30- to 200-nm wavelength range at minimum incident angle of 69.34 deg (dotted lines), central incident angle of 70 deg (solid lines) and maximum incident angle of 70.66 deg (dash lines).

according to experimental measurements. As the angular scans of the samples are performed in *XOY* plane, the divergence in the sagittal direction does not affect the angular resolution in the experiments.

#### 2.2.4 Modulation/monitor chamber

To measure extremely weak reflected beam with the help of lock-in amplifiers, it is necessary to modulate the temporal quasi-continuous light into periodic. For creating periodically modulated light as well as monitoring the light intensity, a two-sector optical chopper disk was mounted in the chamber with Au-coated polished glass cemented on the blades. On the one hand, the periodic signal detected by a groove photoelectric sensor mounted under the blades serves as a reference input for lock-in amplifiers, and the lock-in amplifiers then single out the component of the signal at the reference frequency using a phase-sensitive detection technique so that very small AC signals down to a few pico-amperes can be measured. In our system, the maximum modulating frequency is 60 Hz with the disk rotating 30 revolutions per second. On the other hand, the chopper functions as a beam splitter. The disk chops the light beam at an incident angle of 70 deg, and the reflected reference beam was detected by a Si photodiode (AXUV100G type) to monitor the intensity of the incident beam.

#### 2.2.5 Sample chamber

The sample chamber is a 1.5-m high and 1.2-m diameter chamber housing a high-precision translation stage consisting of a three-dimensional linear stage, an angular stage, and a goniometer assembly with six degrees of freedom which were marked in Fig. 1, including *X* (vertical to the optical path direction in horizontal surface), *Y* (along the optical path direction), *Z* (vertical to horizontal surface),  $\varphi$  (sample inclination),  $\theta_s$  (sample rotation) and  $\theta_d$  (detector rotation), respectively. The  $\theta_s$  and  $\theta_d$  have concentric rotation axis perpendicular to the *XOY* plane with resolution within 4" from 0 deg to 360 deg range. The sample is cemented on a bracket that should be inserted into a fixed slot structure. The sample surfaces were initially parallel to the *YOZ* plane which corresponds to  $\theta_s = 0$  deg. Another twin Si photodiode (AXUV100G type) is used as the detector. The detector was mounted on a rotation arm assembly which was about 430 mm away from the rotation axis and was initially placed at the end of the light beam right behind the sample, which was set as  $\theta_d = 0$  deg, as shown in Fig. 1. The detector can rotate dependently or independently with the sample. *X*, *Y*, and *Z* motions have a resolution of 3  $\mu$ m over its range of  $\pm 50$  mm. The tilt motion controls the sample inclination relative to *Y* axis, and



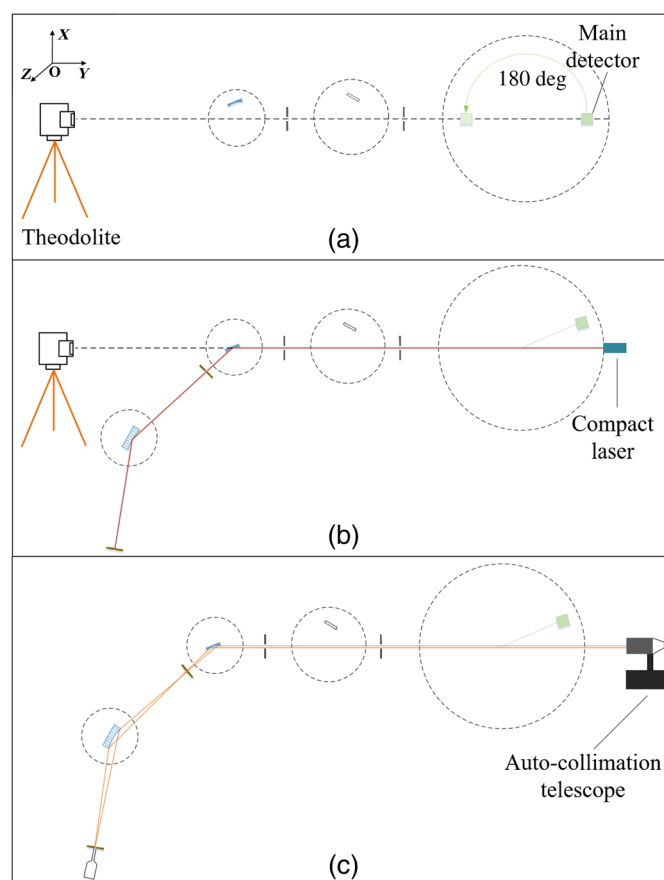
its resolution is better than 3" within the angular range of  $\pm 20^\circ$ . Currently, the samples are cemented on a bracket along Z direction, thus the Z motion can be used to switch the samples. X and Y motions would be applied if the samples need to be translated out of the beam. The stage allows a maximum sample diameter of 100 mm and a weight capacity of 30 kg.

The sample chamber connects with the former chambers by a manual valve. When closing the manual valve, the sample chamber can be vented alone, which is quite convenient for fast changing samples.

### 3 Reflectometer Adjustment

To achieve optimal performance of the reflectometer, precise alignment of the system is necessary. To begin with, a benchmark of the optical axis for subsequent adjustment should be determined.

As shown in Fig. 6(a), the two positions of the detector at 0 deg and 180 deg, respectively, were considered as the datum points to determine the optical axis of the reflectometer, which was then recorded using a theodolite. Afterward, a rough alignment of the system including the chambers and collimation slits was carried out with the help of the theodolite and a compact laser mounted at the end of sample chamber and directed reversely along the optical axis toward the theodolite, as shown in Fig. 6(b). Chambers are connected by bellows which made it possible to shift their positions slightly. Precise alignment was achieved with an auto-collimation telescope, which was located behind the end of sample chamber. Slightly and repetitively adjustments of collimation slits, collimator mirror, slits of monochromator, and the capillary tube of EUV light source were performed progressively, until they all positioned right in the center of the telescope field-of-view, as shown in Fig. 6(c).



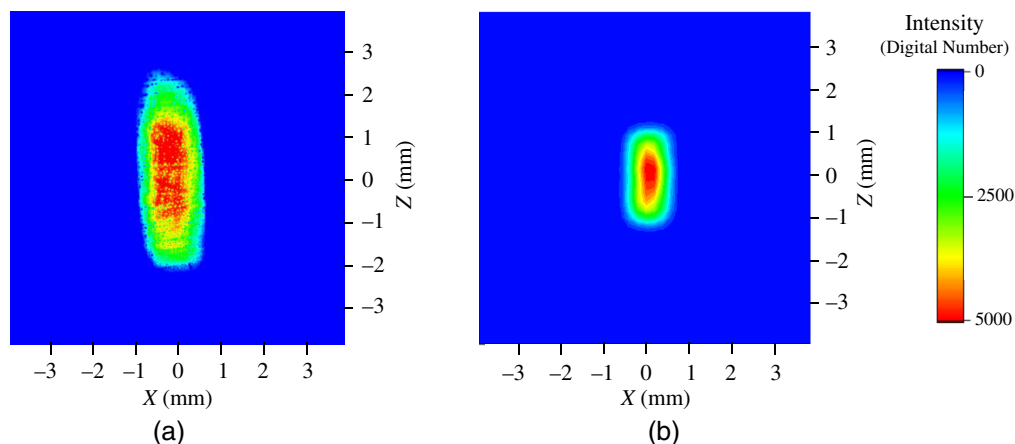
**Fig. 6** Adjustment process: (a) and (b) represent rough alignment with a theodolite and a compact laser, and (c) represents precise alignment with an auto-collimation telescope.



**Fig. 7** Photograph of the system.

The 6D platform of collimator mirror allowed for a final adjustment of the beam direction. The criterion of adjusting the 6D platform is that the reflected beam is nearly parallel in the meridional plane. By precisely adjusting each unit of the system, the detecting beam light intensity can reach an optimal value, and a bright image of the monochromator slit with clear outline and minimal aberration can be acquired. A photograph of the system after adjustment is shown in Fig. 7. All the components of the system are mounted on the frames with supporting structures, each consisting of a wheel and a block that can be switched and locked by a gear-shape valve. During alignment, the wheel is used for flexible moving, and for long-term running, the block is lowered down to maintain stability. The reliability has been corroborated by observing through the above-mentioned UV CCD mounted on the sample chamber.

The measured and simulated light intensity distribution and cross-section size of the beam at the detector position are shown in Figs. 8(a) and 8(b), respectively. The asymmetry of the intensity distribution can be found both in the experimental and simulation results due to the aberrations caused by the gratings and collimating mirror. As for the spot size, the experimental measured spot is about  $1.6 \text{ mm} \times 4.7 \text{ mm}$ , which is larger than simulated spot of



**Fig. 8** 2D-map of the beam profile at the detector position in case of (a) experimental acquired and (b) simulation.



1.3 mm  $\times$  2.5 mm. The quality of the beam is influenced by the slope/figure errors of the gratings and the collimator mirror. In addition, according to the simulation by ZEMAX and the experimental observations, the beam quality is also sensitively affected by the adjustment inaccuracy, such as the position and orientation of the collimator mirror. For this reflectometer, a collimated beam is highly concerned of. So the negative effects of the slope/figure errors and the adjustment inaccuracy can be effectively reduced using two sets of collimation slits to improve the beam quality.

## 4 Experimental Results and System Performance

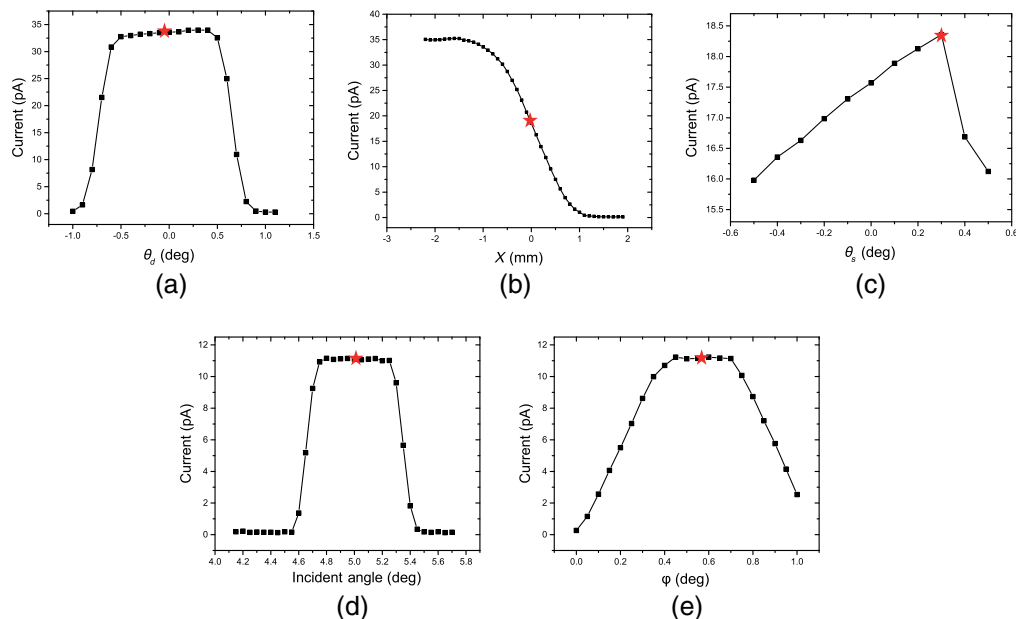
The procedure for the reflectivity measurement includes two steps, the sample orientation alignment and the reflectivity measurements. For testing the performance of this system, two samples of Sc/Si multilayer and Al/LiF/MgF<sub>2</sub> film were chosen. The measurement procedure and reflectivity results will be given as follows.

### 4.1 Sample Orientation Alignment

Adjustment of sample orientation is a necessary step before reflectivity measurements to make sure the sample surface coincides with the rotation axis and the reflected light beam incident on the center of the detector.

There are three steps in general for the sample orientation alignment. First of all, move the sample out of the beam path and scan the detector from  $-1$  deg to  $1$  deg with step of  $0.1$  deg. As shown in Fig. 9(a), the red star at the midpoint of the platform corresponds to  $\theta_d = 0$  deg with respect of probe beam direction.

Secondly, move in the sample along the  $X$  direction perpendicular to the incident beam. Repeatedly move the sample along the  $X$  direction with a step of  $0.1$  mm and rotate around the rotation axis with step of  $0.1$  deg, as shown in Figs. 9(b) and 9(c), respectively, until the sample cut off half intensity of the incident probe beam. The red star in Fig. 9(b) at the half of the slope corresponds to the exact  $X$  value. The red star in Fig. 9(c) shows the maximum intensity where the  $\theta_s$  was set as  $0$  deg. The asymmetry of the light intensity slope in Fig. 9(c) is probably due to the non-uniform intensity distribution of the incident beam, which



**Fig. 9** Sample attitude adjustment. (a)  $\theta_d$  scan, (b)  $X$  scan, (c)  $\theta_s$  scan at initial position, (d)  $\theta_s$  scan at normal incident  $5$  deg, and (e)  $\varphi$  scan.

would cause the sample surface are not in strictly coincidence with the rotation axis and thus the position of the light spot incident on the detector would shift with large rotation angle.

To solve the uncertainty, we need to slightly compensate the offset and calibrate again including the sample rotation angle and inclination at its working angle, to make sure the reflected light beam incident on the center of the photodiode both in the vertical and horizontal direction. Figures 9(d) and 9(e) gives  $\theta_s$  scan around the working incident angle and  $\varphi$  scan for calibrating inclination, respectively. The red stars at the midpoint of the platform in Figs. 9(d) and 9(e) represent the calibrated nominal 5 deg and the exact  $\varphi$  value, respectively.

## 4.2 Sample Reflectivity Measurements

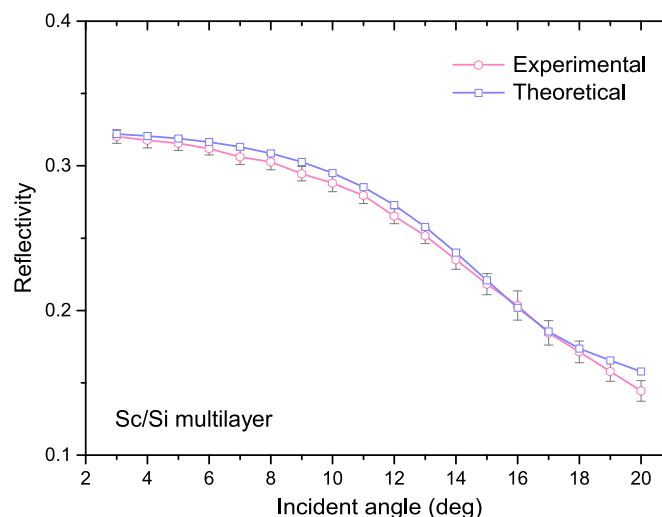
### 4.2.1 Angular dependence of reflectivity

Sc/Si multilayer has excellent reflectivity at the wavelength of 35 to 50 nm and is expected to be applied in the solar EUV telescope for reflecting Ne VII line (46.5 nm) at normal incidence angle.<sup>38</sup> The tested sample was designed as [Si (6.77 nm)/Sc (15.65 nm)]<sub>20</sub>/Si-sub with a top silicon oxide layer estimated to be around 2 nm,<sup>39</sup> to work at 46.5 nm with the normal incidence angle of 4.6 deg. The sample was deposited on a 20 mm × 20 mm polished Si wafer by DC magnetron sputtering and stored with 15% humidity.

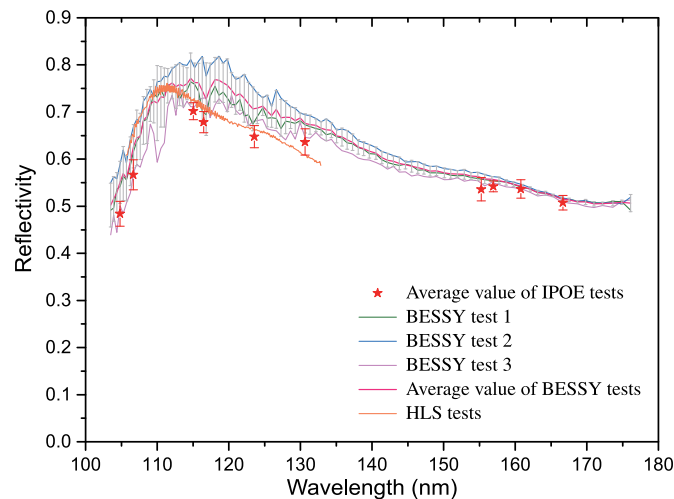
Its angular dependence of the reflectivity was measured and shown in Fig. 10 from 3 deg to 20 deg incident angle with a step of 1 deg. At each angle, both the reflected light intensity and reference light intensity was sampling with 512 Hz and subtracted by background signal. The reflected light intensity was normalized to the reference signal. Theoretical reflectivity calculated by IMD software<sup>40</sup> was also given in Fig. 10 which has preliminarily verified the experimental results were reasonably close to the expected values.

### 4.2.2 Spectral dependence of reflectivity

Al/LiF/MgF<sub>2</sub> film was distinguished by its excellent reflective performance in FUV band thus worth researching for further applications in many astrophysical missions. We have tested a piece of Al/LiF/MgF<sub>2</sub> film sample utilizing relatively strong characteristic line spectrum of several atomic and molecular gases. For calibration, we also measured its reflectivity at BESSY-II synchrotron and HLS, which is given in Fig. 11. Compared with average test value of BESSY-II synchrotron, the deviation is <9%, while compared with tests of HLS, the deviation is <5%. The individually shift deviations may be caused by some very weak spectral lines,



**Fig. 10** Reflectivity curve with changing incident angle from 3 deg to 20 deg.



**Fig. 11** Reflectivity value of Al/LiF/MgF<sub>2</sub> film at different wavelength and compared with tests from BESSY-II and HLS.

consequently, the reflected light intensity would be affected slightly by the fluctuation of the background intensity. At wavelength around 105 nm, results of HLS are relatively unreliable because of the influence of higher diffraction orders.

#### 4.2.3 Stability and repeatability

For verifying system stability, we have performed the same experiment for nine times and acquired a 0.5% RMS value. In addition, with all the experimental conditions unchanged, we carried out the same experiments for days' interval to test system repeatability. Results have demonstrated that the repeatability is better than 2%.

## 5 Summary

The configuration, adjustment, and test results of a reflectometer used for studying optical properties of films in EUV and FUV wavelength band at IPOE laboratory are described. The system mainly consists of an RF-produced gas-discharge light source, a toroidal grazing monochromator, a collimator chamber, a modulation chamber and a sample chamber. After precise and repetitive adjustments of the system, experiments including sample orientation alignments and reflectivity measurements were carried out using the reflectometer.

For testing the performance of this system, we gave an angular scan reflectivity measurement of Sc/Si multilayer and compared the results with theoretical values. We also measured the spectral dependence of reflectivity of Al/LiF/MgF<sub>2</sub> film, then compared the results with test data from BESSY-II and HSL, respectively. The measurement deviation between our system and BESSY-II is <9% while HSL is <5%. Results have proven the stability and reliability of the system with repeatability of 2% and accuracy better than 0.5%. Construction of the reflectometer is expected to obviously shorten the turn-around time of the research and development process of optical coatings at IPOE.

Currently, some spectral lines with much weaker intensity are unable to be applied for reflectivity measurements, and the probe light beam hasn't been linearly polarized yet. In the near future, we plan to substitute the photodiode with channel electron multiplier, so that much weaker characteristic lines and continuous spectra can be used to measure the reflectivity of optical coatings. A four-mirror polarizer will be mounted in the system to produce s-polarized light. At the same time, the probe beam spot on sample surface can be greatly reduced in size which will allow reliable measurements of the samples with relatively large surface peak-valley value.

## Acknowledgments

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